## LIV.—The Equilibrium between Methyl Formate and Methyl Alcohol, and Some Related Equilibria.

By JENS ANTON CHRISTIANSEN.

THE announcement that the Badische Anilin- und Soda-Fabrik had succeeded in synthesising methyl alcohol from carbon monoxide and hydrogen attracted great interest. Patart (J. Ind. Eng. Chem., 1925, 17, 430, 859) claimed priority in this invention; but without entering into this discussion it may be mentioned that the process

$$CH_3 \cdot O \cdot OCH + 2H_2 = 2CH_3 \cdot OH$$
 . . . (1)

patented by the author in 1918, combined with the reaction

$$CH_3 \cdot OH + CO = CH_3 \cdot O \cdot OCH$$
 . . . (2)

investigated by Stähler (*Ber.*, 1914, 47, 580), was the first which made it possible to prepare methyl alcohol from water gas, although any process by which the reaction

$$CO + 2H_2 = CH_3 OH \quad . \quad . \quad . \quad . \quad (3)$$

can be carried out without methyl formate as an intermediate product must be of the greatest value.

The author was able to measure the equilibrium constant of reaction (1) by the kind permission of Prof. E. Billmann, Director of this Laboratory, to whom he wishes to express his thanks. Later, in connexion with a firm in Copenhagen, Mr. Arne Olsen and the author made some measurements of the equilibrium constant of reaction (2). The results of these researches are in this paper : the substance of them was described, with the permission of the firm, in a lecture to the Chemical Society of Copenhagen on October 14, 1924. Earlier work had shown that when methyl alcohol vapour is passed over reduced copper at  $200^{\circ}$  it splits up according to the equation

$$2CH_3 \cdot OH = 2H_2 + CH_3 \cdot O \cdot OCH$$
. . . (-1)

and not, as stated by Sabatier, according to

$$CH_3 \cdot OH = H_2 + CH_2O$$
 . . . . (4)

Before this result was published, Mannich and Geillmann (*Ber.*, 1916, **49**, 585) had drawn the same conclusion. As this reaction (-1) did not appear to be complete, a mixture of measured quantities of hydrogen and methyl formate was passed over reduced copper at about 180°, and a considerable decrease in volume observed, showing the occurrence of reaction (1).

To determine the equilibrium, a stream of electrolytic hydrogen, freed from oxygen by means of palladinised asbestos, and dried, was passed at a constant rate (by the use of a pressure regulator and capillary) through a saturator, containing methyl formate, in a It then passed through a pipette containing reduced thermostat. cuprous oxide on asbestos, which was heated in an electric oven, through two absorption tubes, and into a gas burette. The catalyst was reduced with hydrogen in situ before the experiment. The absorption tubes were filled with N/10-sodium hydroxide. In each experiment, the gas was allowed to escape before reaching the absorption tubes until the rate of flow and the temperatures of the saturator and the oven had been constant for some time. The escape was then stopped and the reaction products were collected. After a suitable time, the absorption tubes were removed and weighed (the hydrogen in them having been replaced by air free from carbon dioxide), and their contents titrated after addition of barium chloride (Winckler's method), so that both methyl alcohol and carbonic and formic acids were determined. The gas was analysed in an Orsat apparatus with platinum capillary. In this way, the amounts of methyl alcohol, methyl formate, hydrogen, carbon monoxide, and dioxide could be estimated. Allowance was made for water lost by evaporation from the absorption tubes, etc.

The equilibrium was also determined by starting with methyl alcohol. This was admitted directly to the catalyst in the oven from a burette through a capillary which was warmed above the b. p. of the alcohol. The results are in Table I, Nos. 1—10 being experiments on reaction (1), Nos. 11—17 on reaction (-1). The temperature of the oven was measured by a standardised thermometer placed outside the catalyst pipette; the error so produced was small, since the rate of flow was slow. The velocities in column 5 are in millimols. of methyl formate or pairs of millimols.

CH. H. H.	amol. mmol. v. p. anal.	5.96 $0.912$ $0.887$	8-60 0-880 0-879	4 0.882 0.864	0-676 0-677	0-676 0-674	97 0-720	0.682	0.689	0.680	707-0	-507	-518	494	444	-522	-511	493
CH. H. H.	amol. mmol. v. p.	5.96 0.912	8-60 0-880	4 0-882	0-676	)·676	67	_			0	0	0	Ò	Ò	0	0	ċ
CH. H.	amol. mmol.	5.96	8-60	4		-	0·0	0.687	0.683	0.672	0.693	0.500	0.500	0.500	0.500	0.500	0.500	0.500
CH.	nmol.			6·6	8-44	5.65	5.25	7-80	6-98	5.49	6.66	7.12	8-00	8.26	4·38	4.16	4.45	7-01
	R		0-17	0.13	0.12	0.15	0.10	0.15	0.13	0.11	0.16	0.12	0.13	0.14	0.05	0.02	0-03	0.04
CO.	mmol.	0.29	0.15	0.22	0.19	0.16	0.13	0.18	0.12	0-11	0.15	0.16	0.15	0.16	0-08	0-08	0.17	0.19
CC	mmol.	<b>4</b> ·38	6.32	5.08	5.04	3.34	3.16	4.68	3.35	2.96	4.09	2.64	2.65	3.11	0-76	0.64	0-34	0.52
HOOOH	mmol.	2-42	3.23	1.54	0-68	0.33	1.145	0.31	3.08	1-48	0-79	0-785	1.34	0.80	1.08	1.42	1.70	2.67
CH.OH.	mmol.	8-29	11-59	7.51	5.03	2.53	5.53	2.86	12-00	6.93	4.85	5.46	6-67	4.83	00-9	6.53	8.22	13.8
Valocity	mmol./hr.	16-9	8-80	2.79	6.86	1.40	4.16	1.85	-5-67	4.29	3.63	2-07	6-05	5.55	2.26	2.37	4.39	5.30
water-	bath.	$13.56^{\circ}$	13.60	13-64	10-60	10-60	10-60	10-60	10-67	10-71	10.70							
in mm.	Hg.	758	773	773	644	179	765	772	776	785	171	785	784	785	787	778	179	774
of name	oven.	198.9°	9-661	198-7	224.8	227-0	197-6	225-5	183-4	192-2	208·3	209-0	214-2	231.2	189-4	195-3	198-9	200-0
	To.	I	2	ŝ	4	5	9	2	œ	6	10	11	12	13	14	15	16	17
	of in mm. water. Velocity, CH. OH. CH. OOCH. CO. CO.	Jemp. Lemp. of Large Velocity. CH <sub>3</sub> .OH. CH <sub>3</sub> .O.OCH. CO. CO. CH <sub>4</sub> . of inm. water. Velocity. CH <sub>3</sub> .OH. CH <sub>3</sub> .O.OCH. CO. CO. Mu No. oven. Hg. bath. mmol./hr. mmol. mmol. mmol. mmol.	Ventry Lensure Lenge Of Action of	Temp. 1 result temp. of         Temp.	No.         Optimum Lemp. or of in mm. water- No.         Velocity. CH <sub>3</sub> ·OH. CH <sub>3</sub> ·OOCH.         CO.         CO <sub>2</sub> .         CH <sub>4</sub> .           No.         oven.         Hg.         bath.         mmol./hr.         mmol.         mmol.         mmol.           1         198-9°         758         13·56°         6·91         8·29         2·42         4·38         0·29           2         199-6         773         13·60         8·80         11·59         3·23         6·32         0·15         0·17           3         198-7         773         13·64         2·79         7·51         1·54         5·08         0·22         0·13	No.       Description relation of in mm. water-value $(H_1, OH, CH_3, OH, CH_3, OOCH, CO, CO_2, CH_4, OH, OH, Hg.       No.       Of in mm. water-value (H_1, H_2, OH, CH_3, OOCH, CO, CO_2, CH_4, OH, OH, Hg.       Constrained (Hg., Hg., Hg., Hg., Hg., Hg., Hg., Hg., $	No.       vertue       temp. of in mm. water.       Velocity. $CH_3$ -OH. $CH_3$ -O.OCH.       CO.       CO_3. $CH_4$ .         No.       oven.       Hg.       Nater.       mol./hr.       mmol.       mmol.       mmol.       mmol.         1       198-9°       758       13-56°       6-91       8-29       2-42       4-38       0-29         2       199-6       773       13-60       8-80       11-59       3-23       6-32       0-15       0-17         3       198-7       773       13-64       2-79       7-51       1-54       5-08       0-22       0-13         4       224-8       779       10-60       6-86       5-03       0-68       5-04       0-19       0-12         5       227-0       779       10-60       1-40       2-53       0-33       3-34       0-16       0-15	No.       vertue       temp. of in mm. water.       Velocity. $CH_3$ -OH. $CH_3$ -O.CH.       CO.       CO_3. $CH_4$ .         No.       ord       in mm. water.       mol./hr. mmol.       mmol.       mmol.       mmol.       mmol.         1       198-9°       755       13-56°       6-91       8-29       2-42       4-38       0-29         2       199-6       773       13-66       8-91       8-29       2-42       4-38       0-17         3       198-7       773       13-64       2-79       7-51       1-54       5-08       0-13         4       224-8       779       10-60       6-86       5-03       0-68       6-04       0-19       0-12         5       227-0       779       10-60       1-40       2-53       0-33       3-34       0-16       0-15         6       197-6       765       10-60       4-16       5-53       1-145       3-16       0-13       0-10	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	No.         vent.         Lemp. of inform.         Velocity. $CH_3$ -OH. $CH_3$ -O.CH.         CO.         CO_3         CH_4.           1         198-9°         758         13-56°         6-91         8-29         2-42         4-38         0-29           2         199-6         773         13-60         8-80         11-59         3-23         6-32         0-15         0-17           3         198-7         773         13-64         2-79         7-51         1-54         5-08         0-15         0-17           4         224-8         779         10-60         6-86         5-03         0-68         5-04         0-19         0-12           5         227-0         779         10-60         1-40         2-53         0-33         3-34         0-16         0-15           6         197-6         765         10-60         2-53         1-145         3-16         0-15           7         225-5         772         10-60         1-85         2-86         0-31         4-16         0-15           7         225-5         772         10-60         1-85         2-86         0-31         4-68         0-16      17         2225-6	No.         vertup. 0.         Velocity. CH3.OH. CH3.OO.CH.         CO.         CO3.         CH4.           No.         oven.         Hg.         bath.         mmol./hr.         mmol.         mmol.         mmol.         mmol.           1         198.9°         758         13.56°         6.91         8.29         2.42         4.38         0.29           2         199.6         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           3         198.7         773         13.64         2.79         7.51         1.54         5.04         0.19         0.12           4         224.8         779         10.60         6.416         3.53         0.33         3.34         0.16         0.15           5         227.0         779         10.60         1.40         2.53         0.33         3.34         0.16         0.15           6         197.6         765         19.60         1.40         2.53         0.33         3.34         0.16         0.15           7         225.6         772         10.60         1.40         2.53         0.33         0.16         0.15 <t< td=""><td>No.         vertup. 0.         Velocity. CH3.OH. CH3.OO.CH.         CO.         CO3.         CH4.           No.         oven.         Hg.         bath.         mnol./hr.         mnol.         mnol.         mnol.         mnol.           1         198.9°         758         13.56°         6.91         8.29         <math>2.42</math> <math>4.38</math> <math>0.29</math>           2         199.6         773         13.60         8.80         11.59         <math>3.23</math> <math>6.32</math> <math>0.15</math> <math>0.17</math>           3         198.7         773         13.64         <math>2.79</math> <math>7.51</math> <math>1.54</math> <math>5.04</math> <math>0.19</math> <math>0.22</math> <math>0.13</math>           4         <math>224.8</math>         779         10.60         <math>1.40</math> <math>2.53</math> <math>0.33</math> <math>3.34</math> <math>0.16</math> <math>0.13</math>           5         227.0         779         10.60         <math>1.40</math> <math>2.53</math> <math>0.33</math> <math>3.34</math> <math>0.16</math> <math>0.12</math>           7         <math>225.5</math>         772         10.60         <math>1.40</math> <math>2.53</math> <math>0.13</math> <math>0.16</math> <math>0.15</math>           7         <math>225.5</math>         772         10.60         <math>1.42</math> <math>2.86</math> <math>0.31</math></td><td><math display="block"> \begin{array}{cccccccccccccccccccccccccccccccccccc</math></td><td>No.         vertup. 0.         followity. CH3.OH. CH3.OO.CH.         CO.         CO3.         CH4.           No.         oven.         Hg.         bath.         mmol./hr.         mmol.         mmol.         mmol.         mmol.           1         198.9°         758         13.56°         6.91         8.29         2.42         4.38         0.29           2         1996         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           3         198.7         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           4         224.8         779         10.60         1.40         2.53         0.58         5.04         0.19         0.12           6         197.6         765         10.40         2.53         0.33         3.34         0.16         0.15           7         225.5         772         10.60         4.16         5.53         1.145         3.16         0.13           7         225.5         772         10.60         1.85         2.86         0.13         0.16         0.15           10         225.5         <t< td=""><td>No.         vertup. 0.         Target water.         Velocity. CH3-OH. CH3-OOCH.         CO.         CO3.         CH4.           1         198-9°         758         13-56°         6-91         8-29         2-42         4-38         0-29           2         199-6         773         13-60         8-80         11-59         3-23         6-32         0-15         0-17           3         198-7         773         13-60         8-80         11-59         3-23         6-32         0-15         0-17           4         224-8         773         13-64         2-79         7-51         1-54         5-04         0-19         0-12           5         227-0         779         10-60         1-40         2-53         0-33         3-34         0-16         0-13           6         197-6         775         10-60         4-16         5-53         1-145         3-16         0-13         0-16           7         225-5         772         10-60         4-16         5-53         1-145         3-16         0-13         0-116         0-13           10         225-5         772         10-60         1-85         2-86         0-13</td><td>No.         vertup. 0.         infinition model.         Velocity. CH3.O.H. CH3.O.OCH.         CO.         CO3.         CH4.           1         198.9°         758         13.56°         6.91         8.29         2.42         4.38         0.29           2         199.6         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           3         198.7         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           4         224.8         779         10.60         6.86         5.03         0.68         5.04         0.16         0.13           5         227.0         779         10.60         4.16         5.53         0.13         4.68         0.16           7         225.6         772         10.60         4.16         5.53         1.145         3.16         0.13           7         225.5         772         10.60         1.85         2.86         0.13         0.16           10         208.3         748         2.79         7.48         2.79         0.13         0.16           11         225.5         772</td><td></td><td></td></t<></td></t<>	No.         vertup. 0.         Velocity. CH3.OH. CH3.OO.CH.         CO.         CO3.         CH4.           No.         oven.         Hg.         bath.         mnol./hr.         mnol.         mnol.         mnol.         mnol.           1         198.9°         758         13.56°         6.91         8.29 $2.42$ $4.38$ $0.29$ 2         199.6         773         13.60         8.80         11.59 $3.23$ $6.32$ $0.15$ $0.17$ 3         198.7         773         13.64 $2.79$ $7.51$ $1.54$ $5.04$ $0.19$ $0.22$ $0.13$ 4 $224.8$ 779         10.60 $1.40$ $2.53$ $0.33$ $3.34$ $0.16$ $0.13$ 5         227.0         779         10.60 $1.40$ $2.53$ $0.33$ $3.34$ $0.16$ $0.12$ 7 $225.5$ 772         10.60 $1.40$ $2.53$ $0.13$ $0.16$ $0.15$ 7 $225.5$ 772         10.60 $1.42$ $2.86$ $0.31$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	No.         vertup. 0.         followity. CH3.OH. CH3.OO.CH.         CO.         CO3.         CH4.           No.         oven.         Hg.         bath.         mmol./hr.         mmol.         mmol.         mmol.         mmol.           1         198.9°         758         13.56°         6.91         8.29         2.42         4.38         0.29           2         1996         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           3         198.7         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           4         224.8         779         10.60         1.40         2.53         0.58         5.04         0.19         0.12           6         197.6         765         10.40         2.53         0.33         3.34         0.16         0.15           7         225.5         772         10.60         4.16         5.53         1.145         3.16         0.13           7         225.5         772         10.60         1.85         2.86         0.13         0.16         0.15           10         225.5 <t< td=""><td>No.         vertup. 0.         Target water.         Velocity. CH3-OH. CH3-OOCH.         CO.         CO3.         CH4.           1         198-9°         758         13-56°         6-91         8-29         2-42         4-38         0-29           2         199-6         773         13-60         8-80         11-59         3-23         6-32         0-15         0-17           3         198-7         773         13-60         8-80         11-59         3-23         6-32         0-15         0-17           4         224-8         773         13-64         2-79         7-51         1-54         5-04         0-19         0-12           5         227-0         779         10-60         1-40         2-53         0-33         3-34         0-16         0-13           6         197-6         775         10-60         4-16         5-53         1-145         3-16         0-13         0-16           7         225-5         772         10-60         4-16         5-53         1-145         3-16         0-13         0-116         0-13           10         225-5         772         10-60         1-85         2-86         0-13</td><td>No.         vertup. 0.         infinition model.         Velocity. CH3.O.H. CH3.O.OCH.         CO.         CO3.         CH4.           1         198.9°         758         13.56°         6.91         8.29         2.42         4.38         0.29           2         199.6         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           3         198.7         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           4         224.8         779         10.60         6.86         5.03         0.68         5.04         0.16         0.13           5         227.0         779         10.60         4.16         5.53         0.13         4.68         0.16           7         225.6         772         10.60         4.16         5.53         1.145         3.16         0.13           7         225.5         772         10.60         1.85         2.86         0.13         0.16           10         208.3         748         2.79         7.48         2.79         0.13         0.16           11         225.5         772</td><td></td><td></td></t<>	No.         vertup. 0.         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CH4.           1         198-9°         758         13-56°         6-91         8-29         2-42         4-38         0-29           2         199-6         773         13-60         8-80         11-59         3-23         6-32         0-15         0-17           3         198-7         773         13-60         8-80         11-59         3-23         6-32         0-15         0-17           4         224-8         773         13-64         2-79         7-51         1-54         5-04         0-19         0-12           5         227-0         779         10-60         1-40         2-53         0-33         3-34         0-16         0-13           6         197-6         775         10-60         4-16         5-53         1-145         3-16         0-13         0-16           7         225-5         772         10-60         4-16         5-53         1-145         3-16         0-13         0-116         0-13           10         225-5         772         10-60         1-85         2-86         0-13	No.         vertup. 0.         infinition model.         Velocity. CH3.O.H. CH3.O.OCH.         CO.         CO3.         CH4.           1         198.9°         758         13.56°         6.91         8.29         2.42         4.38         0.29           2         199.6         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           3         198.7         773         13.60         8.80         11.59         3.23         6.32         0.15         0.17           4         224.8         779         10.60         6.86         5.03         0.68         5.04         0.16         0.13           5         227.0         779         10.60         4.16         5.53         0.13         4.68         0.16           7         225.6         772         10.60         4.16         5.53         1.145         3.16         0.13           7         225.5         772         10.60         1.85         2.86         0.13         0.16           10         208.3         748         2.79         7.48         2.79         0.13         0.16           11         225.5         772		

TABLE I.

METHYL FORMATE AND METHYL ALCOHOL, ETC. 415

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alcohol passing the catalyst per hour. Columns 12 and 13 give the initial ratio in molecules of ester to hydrogen, and are calculated (1) from the vapour pressure of the ester and the total pressure in the saturator, (2) from the analysis of the products; in the decomposition experiments the ratio should obviously be 0.500. These values give a check on the analyses, and show a satisfactory agreement. The values in the last column are those of the constant  $K_1 = C^2_{\rm H_2}C_{\rm CH_2OCH}/C^2_{\rm CH_2OH}$ .

The values of  $\log_{10} K_1$  (expts. 1—15) are plotted in Fig. 1 against 1/T; they show that the results of association and dissociation experiments lie on the same curve, proving that true equilibrium was reached. The values of  $K_2$  for the reaction  $CH_3$ ·O·OCH = CO +  $CH_3$ ·OH were so discordant as to show that equilibrium had not



been reached. The values obtained from expt. 15 (Fig. 1) and expts. 16 and 17 (not plotted) lie well below the curve; evidently the catalyst, which was the same in all these experiments, had lost its activity, so that even the equilibrium  $(\pm 1)$  was not now attained.

The values for  $CO_2$  and  $CH_4$  in the table suggest that the reaction

$$CH_3 \cdot O \cdot OCH = CO_2 + CH_4 \quad . \quad . \quad . \quad (5)$$

took place to a slight extent. If, however, a trace of water was present, carbon dioxide may have been formed by the reaction

(J. Amer. Chem. Soc., 1921, 43, 1670); this would explain the excess of carbon dioxide found in some of the experiments.

The equilibrium constant of reaction (2) was determined in a

similar manner and in the same apparatus. The catalyst here was solid sodium methoxide. This absorbed some carbon monoxide, and hence the results are not very trustworthy. The same thing occurred, but to a much smaller extent (about 1 mol. of sodium methoxide disappearing for every 100 mols. of carbon monoxide converted into methyl formate), when the reaction was carried out in solution, and in this case the reaction causing the carbon monoxide to disappear was shown to be  $CH_3 \cdot O \cdot OCH + NaO \cdot CH_3 = CH_3 \cdot O \cdot CH_3 + NaO \cdot OCH$ . Hence the values of the equilibrium constant  $K_2$  are only to be regarded as preliminary, but those of the association and dissociation experiments agree fairly well, as the following table shows.

## TABLE II.

	_	$\operatorname{Log} K_{2}$ by	$\operatorname{Log} K_2$
Reaction.	Temp.	exper.	calc.
(-2)	102°	1.82	Ī∙81
(2)	74	Ī·53	Ī·40
(-2)	74	Ī·40	Ĩ∙40
(-2)	70	<b>Ī</b> ∙29	Ī·34

 $K_2 = C_{\rm CO}$ .  $C_{\rm CH_3-OH}/C_{\rm CH_3OOCH}$  is for the gas mixture leaving the catalyst. The values in column 4 are calculated by the equation  $\log_{10}K_2 = -$  1880/T + 4.82.

The effect of temperature on equilibrium should be accurately given over a fairly wide range by an expression of the form

$$\log_{10} K = -A/T + B,$$

where A = heat of reaction at constant volume divided by 4.571, and B is a constant (Scheffer, *Proc. K. Akad. Wetensch. Amsterdam*, 1917, **19**, 636). Values calculated on this formula are in Table II and are represented by the straight line in Fig. 1. The values given in the literature for the heats of combustion of methyl alcohol and methyl formate are discordant, Stohmann's value for methyl alcohol being about 2 Cals. lower than that of Thomsen. I have preferred to use the latter, since, although Thomsen's "universal burner" is apt to give somewhat high values, the error may be expected to be small when the substances are volatile, whilst, on the other hand, Stohmann's values, according to Roth (*Z. Elektrochem.*, 1911, **17**, 789), may be suspected to be low, especially in the case of volatile liquids.

The heat capacity of methyl alcohol has been calculated from the values in Landolt-Börnstein's tables for the ratio, k, between the two heat capacities. For methyl formate, no direct data seem to be available, but from the value for ethyl formate and those for methyl and ethyl alcohols the heat capacity of methyl formate (at constant volume) has been estimated at 10 cals. per degree.

The following table contains all the numerical values used in the calculation of the reaction heats at the temperatures in question.

Substance.	Heat of combustion at const. press.	Heat capacity at const. vol.
Methyl alcohol	182,230	7.8
Methyl formate	241,210	10.0
Carbon monoxide	. 67,960	5.0
Hydrogen	68,430	4.8

By means of this table the heat of reaction (1) at constant volume and about 200° is calculated to be 13,800 cals. and that of reaction (2) at about 100°, 8,600 cals. From these values and the above determinations of the equilibrium constants, the constants, B, of reactions (1) and (2) can be calculated as 3.61 and 4.82, respectively. These two numbers thus contain the results of the above investigation of the two reactions.

It is now possible to obtain from Fig. 1 and Table II a preliminary value of the equilibrium constant  $K_3 = C_{\rm CO} \cdot C^2_{\rm H_3}/C_{\rm CH_3 \cdot OH}$  for the reaction (3). Calculation shows that

From (7) it can be calculated that at about 200°  $K_3$  is about 10<sup>-2</sup>, so that at this temperature, if the hydrogen concentration is 1 mol. per litre, only 1% of the carbon monoxide will remain if the reaction  $2H_2 + CO = CH_3 \cdot OH$  proceeds until equilibrium has been reached, whilst, on the other hand, if the hydrogen concentration is 0.01, only 1% of the carbon monoxide will be transformed into methyl alcohol.

The value of  $K_3$  can also be roughly predicted by means of one of the well-known approximate equations arrived at from Nernst's third law of thermodynamics, for instance, the one given by Nernst himself,

$$\log K_p = -Q_{18}/4.57T + 3.5 \log T + 2i_{\rm H_s} + i_{\rm CO} - i_{\rm CH_s \cdot OH}$$
(8)

where the *i*'s are the so-called conventional chemical constants of the different molecular species.

As shown by Cederberg (*Dissert.*, Upsala, 1916), a close connexion seems to exist between the critical pressure of a substance and its chemical constant and therefore I have used the values  $i_{\text{H}_4} = 1.6$ ;  $i_{\text{CO}} = i_{\text{N}_2} = 2.6$ ;  $i_{\text{CH}_3 \cdot \text{OH}} = i_{\text{SO}_2} = 3.3$  (see Pollitzer, Ahrens's Sammlung 17, 1912).

By means of  $K_p = (RT)^2 K_c$  and the data just mentioned we thus find

$$\log K_3 = -22700/4.57T + 1.5\log T + 4.7$$
 . (8, i)

As furthermore  $1.5 \log T$  at temperatures about  $200^{\circ}$  is very nearly equal to 4.0, the equation becomes

$$\log K_3 = -4966/T + 8.7$$
 . . . (8, ii)

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The agreement (see Fig. 2) between (8, ii) and (7) is as good as could be expected, considering the preliminary character of the investigation of reaction (2) and the approximations implied in the use of the Nernst equation (8).

By combining equation (7) with a similar relation derived from earlier experiments on the reaction

$$H_2O + CO = CO_2 + H_2$$
 . . . . (9)

it is furthermore possible to calculate the equilibrium constant of the reaction (6). If we define  $K_g$  by means of the equation  $K_g = C_{\text{H}_2\text{O}} \cdot C_{\text{CO}} \cdot C_{\text{CO}} \cdot C_{\text{H}_2}$ , where the concentrations are those at equi-



librium, we get from Hahn's experiments (Z. physikal. Chem., 1903, 44, 513; 1904, 48, 735; see Haber, "Thermodynamik technischer Gasreaktionen," Berlin, 1905)

$$\log_{10} K_9 = -1854/T + 1.66$$
 . . . (10)

When this equation is subtracted from (8, ii) we obtain

$$\log_{10} K_6 = -3042/T + 6.77$$
 . . (11)

where  $K_6$  is the equilibrium value of  $C_{CO_2}$ .  $C^{3}_{H_2}/C_{CH_3 \cdot OH}$ .  $C_{H_2O}$ .

and

Finally it should be remarked that by means of existing data on the equilibria

$\mathrm{C}+2\mathrm{H_2}=\mathrm{CH_4}$	•	•	•	•	•	•	(12)
$C + CO_2 = 2CO$							(13)

and the equations given above, it should also be possible to calculate the value of the equilibrium constant for the reaction (5).

The first of these reactions has been investigated by Mayer and

Altmayer (Ber., 1907, 40, 2134), Coward and Wilson (J., 1919, 115, 1380), and Pring and Fairlie (J., 1912, 101, 91). The results of these authors may be represented with sufficient accuracy by means of the equation

$$\log K_p = \log \frac{p_{\text{CH}_4}}{p^2_{\text{H}_3}} = \frac{5450}{T} - 6.33 \quad . \quad . \quad (14)$$

If we wish to get  $K_c = C_{CH_t}/C^2_{H_s}$  with the concentrations expressed in mols. per litre, we must add  $\log RT = \log T - 1.09$  and consequently

$$\log K_{e} = 5450/T + \log T - 7.42$$
 . . (14, i)

For the reaction (14) a summary of the existing data is to be found in a paper by Jellinek and Diethelm (Z. anorg. Chem., 1922, 124, From their table of the mean values of  $K_p$  found at different 220).temperatures by different authors, the following expression may be calculated :

$$\log K_p = 8620/T - 8.80$$
 . . . (15)

and transforming into  $K_{c}$ ,

$$\log K_e = \log \frac{C_{co_e}}{C_{co}^2} = \frac{8620}{T} + \log T - 9.89$$
 . (15, i)

By adding these equations we get the equilibrium constant for the reaction  $2H_2 + 2CO = CH_4 + CO_2$ , viz.,

$$\log K_p = \log \frac{p_{\text{CH}_4} \cdot p_{\text{CO}_8}}{p_{\text{H}_8}^2 \cdot p_{\text{CO}}^2} = \frac{14070}{T} - 15.13 \quad . \quad . \quad . \quad (16)$$

or 
$$\log K_{e} = \log \frac{C_{\text{CH}_{4}} \cdot C_{\text{CO}_{5}}}{C^{2}_{\text{H}_{4}} \cdot C^{2}_{\text{CO}}} = \frac{14070}{T} + 2\log T - 17.31$$
 (16, i)

Adding to this the equation (7), we get the logarithm of the equilibrium constant for the reaction  $CH_3 \cdot OH + CO = CH_4 + CO_2$ , viz.,

$$\log K_{s} = \log \frac{C_{\text{CH}_{s}} \cdot C_{\text{CO}_{s}}}{C_{\text{CH}_{s}} \cdot \text{OH} \cdot C_{\text{CO}}} = \frac{9170}{T} + 2\log T - 8.88 \quad . \quad (17)$$

from which it is evident that the formation of methyl alcohol from methane and carbon dioxide will take place only at temperatures at which methane is not at all stable, whilst it is possible, according to equations (11) and (7), to obtain reasonable amounts of methyl alcohol from hydrogen and either carbon monoxide or dioxide at not too high temperatures.

It is obvious that the equations given above all contain the uncertainty introduced by the use of the preliminary results for the equilibrium between carbon monoxide, methyl alcohol, and methyl formate.

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## Summary.

(1) The equilibrium constant of the reaction  $CH_3 \cdot O \cdot OCH + 2H_2 = 2CH_3 \cdot OH$  has been determined with fair accuracy at temperatures in the neighbourhood of 200°.

(2) Preliminary values for the equilibrium constant of the reaction  $CH_3 \cdot OH + CO = CH_3 \cdot O \cdot OCH$  at about 100° have been given.

(3) It is shown that by combination of the found values with existing data the equilibrium constants of the reactions  $CO + 2H_2 = CH_3 \cdot OH$ ;  $CO_2 + 3H_2 = CH_3 \cdot OH + H_2O$ ; and  $CH_4 + CO_2 = CH_3 \cdot OH + CO$  may be calculated.

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